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### Azur 840C Up-sampling CD player

Matthew Bramble, Cambridge Audio Thierry Heeb, Anagram Technologies Tim Llewellynn, Anagram Technologies



The 840C up-sampling CD player is part of Cambridge Audio's flagship '8' series range, designed to match our 840A Class XD<sup>™</sup> integrated amplifier itself the subject of a white paper and patent-pending amplifier technology.

#### Background

When we considered a matching CD player we examined the necessary factors that make a truly great CD player – imaging, timing and overall sound quality. By dissecting each in turn we came up with a technological shopping list for the 840C.

Incredibly high quality DACs would of course be required. For best stereo imaging properties it was decided that two would be used, one for the left channel and one for the right, this would allow for discrete circuits for the very best channel separation. In addition the circuits could then be made symmetrical, giving them identical properties, further improving imaging. If two DACs were used we could exploit the benefit of dual differential mode, reducing distortion and allowing a true balanced output. DC servos could be used allowing no capacitors at all in the signal path. Lastly if we could use a DSP to process the data we could perform our own digital filtering, jitter suppression and even up-sampling to a higher sample rate, ideally combining this with a superior output filter using a Bessel topology with constant group delay and linear phase, the best kind of filter to use with excellent timing characteristics.

#### The completed wish list was:

- Upsampling and jitter suppression via DSP
- Twin dual differential 24-bit DACs
- DC coupled outputs with DC servos
- Fully balanced filter topology

24/384 PSAMPL



• Linear phase Bessel filters for constant group delay

In order to achieve the above we needed to find an upsampling technology which would meet our needs. As luck would have it around this time we met Anagram Technologies of Switzerland who had long been offering upsampling algorithm and modules for some very high end manufacturers.

Anagram was keen to work with us and agreed to even customise and license their code to us for inclusion in our own DSP. After careful consideration and critical evaluation of all options, we decided on a BF352 32 Bit 'Black Fin' DSP from Analog Devices, running a custom version of their patented ATF<sup>™</sup> (Adaptive Time Filtering) upsampling process known by Anagram as Q5<sup>™</sup> Upsampling.

#### **Q5™ Upsampling with ATF™**

Key to the success of the 840C is a technology called ATF. ATF is a resampling process that allows audio data to be interpolated at a higher precision than standard techniques used in off-the-shelf sample rate converters. ATF uses an advanced polynomial curve fitting algorithm that closer matches the original audio data, than sample-and-hold, or piece-wise linear estimation interpolators, commonly used today. This advanced technique allows jitter invoked errors in the resampling process to be minimized to a point where they no longer become relevant, and as this process is extremely efficient, ATF allows Q5 Upsampling to be implemented on a relatively low cost DSP. Critically this has enabled Cambridge Audio to bring this high-end technology to a new midrange price level.

Standard interpolators are of two types, sample-and-hold, or piece-wise linear and typically have a maximum output signal sampling frequency limited to 192kHz. The diagram below shows a comparison between normal upsampling and Q5 Upsampling running at 384kHz using ATF in the theoretical case where all clocking is jitter free. In the following diagrams we will show how ATF provides superior performance in the presence of jitter and how it minimizes the impact of resampling jitter.

### White paper



The first thing to notice between ATF and other interpolators is the error path between output samples. This error path in a sample-and-hold interpolator will have a path that does not follow the original sample data, as shown below. In the case of ATF, the error path is determined by the **smooth curve fitting algorithm**, which recalculates a new path every sample, resulting in a path that closely follows the original audio input data.



Having an error path that closely matches the original data will have two benefits: resampling errors caused by jitter appearing on data clocks and by using arbitrary non integer sample rates e.g. 44.1kHz to 48kHz will be minimized. In the case of Q5 the **extremely small residual error which remains** is designed to be beyond the dynamic range of 24-bit audio which is far superior to that of sample-and-hold or piece-wise linear interpolators.



Jitter in the incoming data clock will cause upsampled data points to move along the error path where errors in the sample rate conversion resampling give rise to distortion in the audio data

Performing a frequency domain analysis of the resampling error invoked by data jitter or arbitrary non integer sample ratios we find that ATF has some interesting properties. Firstly since ATF is a

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non-linear process, **resampling errors are uncorrelated with amplitude**, which is not the case with the sample and hold interpolator, and secondly due to the smooth time domain function of ATF, error harmonics will be greatly reduced.



**High jitter error** harmonics due to piece-wise hold error path, typical performance that does not exceed **-110 THD+N** and if higher performance is required it can not run on low cost DSPs.



Low jitter error harmonics due to natural curve fitting leading to better than -144dB THD+N for asynchronous sample rate conversion that can run on low cost DSPs.

#### What is jitter?

The basis of digital audio theory is Shannon's sampling theorem. It states that a signal may be completely recovered by its samples, provided the sampling rate is at least twice the highest frequency present in the signal. One key assumption of Shannon's sampling theorem is that the sampling is uniform, i.e. the sampling rate is constant (fixed sampling period Ts(n) = Ts) as shown in Figure 1.



Figure 1: Uniform sampling according to Shannon's theorem.

Jitter is defined as the deviation from uniform sampling or, in other words, as the time fluctuations of the sampling period. The general model for a jittered sampling signal is given by:

Ts(n) = Ts + e(n) where e(n) is a zero-mean random process.



This introduces time domain distortion as the sampling instants are moved from their intended position. Jitter based distortion is particularly harmful for audio quality as the human ear is especially sensitive to timing errors. Indeed the human ear relies on time domain information to locate events in space-time. Jitter therefore blurs the timing information of the reproduced audio signal, resulting in surprisingly degraded audio quality.

Jitter also introduces amplitude modulation products into modern DACs particularly bitstream types which rely on the intrinsic timing of the individual data packets to determine each conversion of the bitstream, these DACs whilst they can provide an excellent musical performance need very careful control of their time domain behaviour.

Assuming already very good Total Harmonic Distortion performance (as is now the norm with most well designed audiophile CD players) jitter is arguably now the most detrimental form of distortion in digital audio playback and recording systems.

Figure 2 shows the same signal portion as above except with exaggerated jitter to illustrate clearly the resulting distortion.



Figure 2: Non-uniform sampling resulting from jitter.

#### Where does jitter appear?

As no perfect components exist, jitter is in fact present in any digital circuit. It already originates in the system's oscillator where non-perfect switching electronics contribute to it. Jitter is also created by circuit traces acting like antennas picking up noise from all kind of noise sources in the design or generated by component imperfections or thermal noise. Jitter is also introduced where imperfect power supplies allow the switching thresholds of digital ICs to be modulated. Reflections

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in imperfectly terminated high frequency traces or signal wires cause ringing which also introduces jitter. Finally jitter can be introduced by the data itself. Capacitance in traces and other effects allow the switching threshold of the ICs to be modulated by the very data itself, a phenomenon known as data related jitter.

Therefore jitter is a natural element of every real world digital circuit design. The trick as ever is to minimise it at source and crucially to remove it at the conversion point from the digital to analog domain as will be seen later.

### How do we reduce jitter?

Firstly a good understanding of the causes of jitter as above allows a lot of jitter sources to be minimised at source. The 840C in common with other Cambridge Audio CD players uses a high precision master clock, careful control of high frequency signal lines for impedance, cross-talk and a raft of other careful design considerations.

But with these all in place there is an inevitable small amount of jitter left that we wanted to eliminate for the very best performance possible. The 'traditional' way to do this in a high end CD player is with a Phase Locked Loop (PLL) or Sample Rate Converter (SRC).

PLLs are often used to "de-jitter" a signal by driving a Voltage Controlled Crystal Oscillator (VCXO) to be synchronous to a given clock source.

For a PLL solution a high accuracy VCXO master clock is used to clock the audio data into the DAC. This clock is then locked to the average rate of the incoming data which is also buffered. The idea is to split the timing of the outgoing data from that going in so that the jitter in the outgoing data is determined purely by the new accurate master clock.

However to avoid loss of samples when the two clocks are asynchronous the data is buffered (usually in RAM) and the master clock made variable so that its average rate matches the incoming rate. To do this PLLs rely on comparator and loop filter to compare the timing of high accuracy master clock with the incoming clocks.



Fig 3. General scheme of a PLL based circuit

The size of data buffer and loop filter must be carefully chosen and actually determines the lowest frequency of jitter that can be suppressed. Commercial designs usually end up with a cut-off point of about 1kHz. However this means that a large amount of low frequency jitter gets through.

Another method used by some is to use an off-the-shelf sample rate converter (SRC) I.C. In this case the SRC replaces the RAM buffer and other components and acts as the time bridge between input and local clock domains.

Most high quality SRCs currently available on the market employ a digital filter that provides the function by first up-sampling the data to a very high sampling rate followed by down-sampling to the required different output sampling rate. A PLL function and buffering is usually done in the digital domain.

As SRCs as well as allowing jitter suppression can allow different input and output clocks, upsampling can be achieved. This is done by simply setting the output frequency at a fixed higher rate than that which is coming in.







However using an SRC whilst it would indeed have provided a measure of jitter suppression and allowed us to interpolate the incoming data to 24-bit and 192kHz isn't the best that can be done.

For one, we would have been restricted to 192kHz. SRC chips are typically aimed at pro-audio implementations where the data is transmitted/received over S/PDIF. The maximum sample frequency SPDIF supports is 192kHz.

In order to allow the use of a low order filter topology, the higher the sample frequency the better. Using our own DSP based solution would allow higher sample rates to be achieved, 384kHz in the case of the 840C. Also the sophisticated curved fitting and other technologies uses in the ATF process provide real benefits in terms of both sonic and measured qualities as will be seen later.

### Where does jitter matter?

Jitter actually only matters at the digital to analogue (or analogue to digital) conversion stage. As long as a signal remains in the digital domain and satisfies all electrical timing specifications, jitter is of no concern. If it did, it would be impossible to listen to any music stored on a computer's harddrive as data transmission to the main processor and then to the audio section is packet based

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without any reference to a real clock source. Only at playback when audio is streamed through the D/A converter does timing information, and hence jitter, matter.

Digital to analogue conversion is often considered (or defined) as the conversion from discrete domain data into continuous domain data. However we think this definition lacks one important point which is time. Thus an extended definition of digital to analog conversion could be the conversion of data from a discrete domain into continuous domain data and the conversion from abstract time to real-world time. Indeed when stored as pure digital information (such as on a CD/DVD or on a hard-drive) the audio data file only carries symbolic information about the content's sampling rate; while in this form, it has no relation with a real-time base.

#### Jitter at the digital to analogue domain boundary

The task of a digital to analogue (or analogue to digital) converter is twofold: conversion of discrete symbolic data (binary code) to continuous real data (electrical current or voltage) and the conversion of abstract-time to real-world time, basically some kind of synchronisation.

Incorporated in Anagram's patented Q5 Upsampling is a form of synchronisation called DSS<sup>™</sup> (Data to System Synchronisation). Instead of adapting the system's operating frequency to the incoming time base or to use a RAM buffer or an SRC chip, DSS<sup>™</sup> uses a software based upsampler (sample rate converter) based on their Q5<sup>™</sup> SRC kernel to perform abstract to real-world time conversion using a local high quality single clock.

The fact that all clocks in the system are made synchronous to this local high quality clock is one of the key aspects of DSS<sup>™</sup>. As such the DSP and all other clocked devices in the system are driven using a clock derived synchronously from this local clock source. The general idea behind DSS<sup>™</sup> is to use a single time base and to adapt the audio data to this time base result in the extraordinary jitter rejection performance seen in the implementation of this technology. Furthermore, the complete system being synchronous, possible noise appearing in the output stage and resulting from multiple clocks interaction is reduced to a minimum.



Figure 8 shows the structure of a DSS<sup>™</sup> synchronisation based digital audio playback unit.

See below for a real world comparison of the output of the 840C's up-sampling DSP and a well know competing SRC.



So we have seen that the 840C's up-sampling technology can give a very smooth high resolution up-sampled digital audio waveform with low distortion which can be used to eke the very best performance from modern 24-bit DACs. The idea being to use the artificially higher resolution data created to get as close as possible to the true 16-bit performance of the CD disc, in our case we chose to use two AD1955 24-bit DACs from Analog Devices. These are very high end products

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giving excellent performance with the advantage of true balanced outputs. Finally the process also had another big advantage for us in that the high sampling frequency could allow us to use a special filter topology for the output stage with many advantages.

#### The 840C's anti-aliasing / reconstruction filter

The 840C uses a Linear Phase Bessel output filter, arguably the best possible type of filter for audio use. However these filters are rarely seen in audio equipment as the filter response has quite slow roll off in the frequency domain.

The term Bessel refers to a type of filter response, not a type of filter. It features flat group delay in the passband:



This is the characteristic of Bessel filters that makes them valuable to designers. Very few filters are designed with high slew rates or square waves in mind. Most of the time, the signals filtered are sine waves, or close enough that the effect of harmonics can be ignored. If a waveform with high harmonic content is filtered, such as a square wave, the harmonics can be delayed with respect to the fundamental frequency if a Butterworth or Chebyshev response is used. The Fourier Series of a square wave is:

$$x(t) = \sin(\omega_{o}t) + \frac{\sin(3\omega_{o}t)}{3} + \frac{\sin(5\omega_{o}t)}{5} + \dots$$

This means that a square wave is an infinite series of odd harmonics, or sine waves, summed together to create the square shape. Obviously, if a square wave is to be transmitted without distortion, all of the harmonics - out to infinity - must be transmitted. This means that the square wave can be high pass filtered without distortion, if the 3 dB point of the filter is significantly lower © Cambridge Audio 2006 Version 1.0

## White paper

than the fundamental. If the square wave is low pass filtered, however, the situation changes dramatically. Harmonics will be eliminated, producing distortion in the square wave. It is the job of the designer to decide just how many harmonics must be passed and what can be eliminated. Suppose that the designer wants to keep five harmonics. The resulting waveform looks something like this:



This may be acceptable to the designer - it depends on the timing of the leading and trailing edge of the waveform. The elimination of harmonics will result in rounding of the edges, and therefore delay in the leading and trailing edges of the digital signal. Of more importance, the harmonics that are passed will not be delayed.

The Bessel approximation also has a very smooth passband and stopband response, like the Butterworth. However for the same filter order, the stopband attenuation of the Bessel approximation is much lower that that of the Butterworth approximation. See below:



This is the issue that often precludes its use. Aliasing noise inherent in sampled digital audio will be less attenuated by a Bessel filter than other types. However if the aliasing can be moved up in frequency to be well out of the audio range and within the range where the Bessel filter does apply good attenuation this problem can be solved.

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The 840C by applying 384kHz up-sampling does exactly this.

It should also be noted that there is no ripple in the passband of a Bessel filter.

The phase response of the three filter types is now shown below. The Bessel response also has the slowest rate of change of phase.



So the Bessel topology has been shown to have minimum ripple in the pass band, slowest rate of change of phase and constant group delay in the pass band. All these features make it perfect for audio use if its relatively slow roll off can be accommodated, in the 840C we were able to do this happily by up-sampling all audio to 384kHz in DSP.

#### **Other features**

Two digital inputs are fitted allowing other digital sources to be connected directly to the 840C and up-sampled, the 840C then operates as a very high quality DAC.

A digital output is also fitted which can even output upsampled data at various rates and word widths, independent from the main audio output, which is always set at 24/384 for best sound quality.

In addition to these audiophile features, Control Bus Input/Output, IR Emitter Input and RS232 control are provided to make it easy to integrate the 840C into custom installation systems if desired.



#### **Technical specifications**

D/A Converters		Dual An	Dual Analog Devices AD1955 24bit DACs		
Digital Filter	Analog Perforn	Analog Devices BlackFin ADSP-BF532 32bit DSP Performing Q5 Upsampling to 24bits 384kHz			
Analog Filter 2 Pole Fully Differential Linear Phase Bessel filter					
Frequency res	ponse	20Hz to 20kHz	(+/-0.	1dB)	
THD @ 1Khz 0	dBFs	< 0.0008%			
THD @ 1Khz -10dBFs < 0.0005%					
THD @ 20Khz 0dBFs < 0.006%					
IMD (19/20kHz) 0dBFs < 0.0006%					
Linearity @ -90	DdBFs	+/- 0.5dB			
Stopband rejection (>24kHz) > 115dB					
S/N ratio, A weighted > 113dB					
Total correlate	d jitter	< 130pS			
Crosstalk @1k	Hz	< -130dB			
Crosstalk @20	)kHz	< -110dB			
Output impeda	ance	< 50 ohms			
Input words widths supported 16 - 24bit					
Output words widths supported 16, 20, 24bit					
Input sampling frequencies supported 3 192kHz			I	32kHz, 44.1kHz, 48kHz, 88.2kHz, 96kHz, 176.4kHz,	
Ouput sampling frequencies supported 32kHz - 192kHz pass through (Including 44.1kHz for CD) 48kHz, 96kHz, 192kHz upsampled					



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